

Introduction of Dislocation-mediated Plasticity and Discrete Dislocation Dynamics

Department: Mechanical Engineering

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Outline

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 - 1.2 Polycrystalline
 - 1.3 Critical Shear Stress
2. Dislocation
 - 2.1 Definition and Burger Vector
 - 2.2 Force on Dislocation
 - 2.3 Mobility and Interaction
 - 2.4 Dislocation Generation

Part 2 Dislocation Study

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2. Simulation: Multiple Approaches

Part 3 Discrete Dislocation Dynamics(ParaDis)

- 3.1 Basic Calculation Principle
- 3.3 Dislocation Mobility
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Part 4 Preliminary Results

- 4.1 Frank-Read Dislocation Source
- 4.2 Aluminum Constant Strain Rate
- 4.3 Aluminum Constant Stress

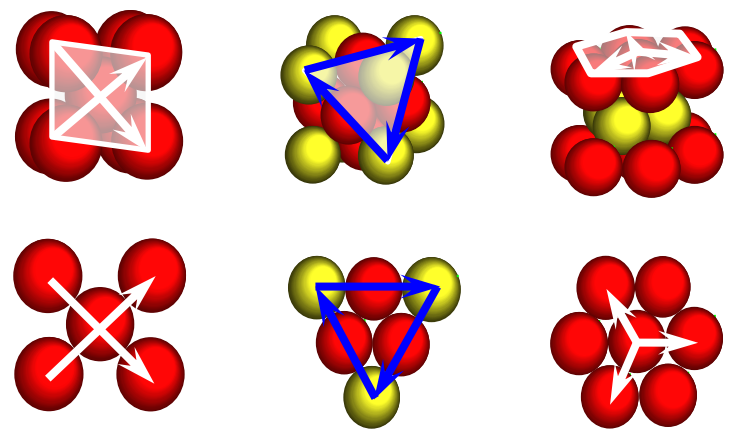


Part 1 Dislocation-mediated Plasticity

1. Plasticity Deformation

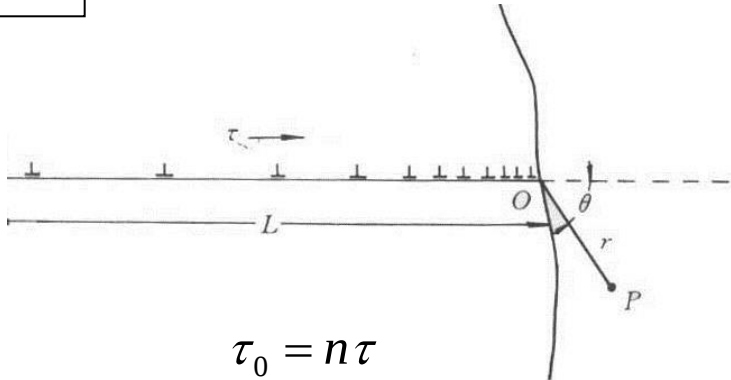
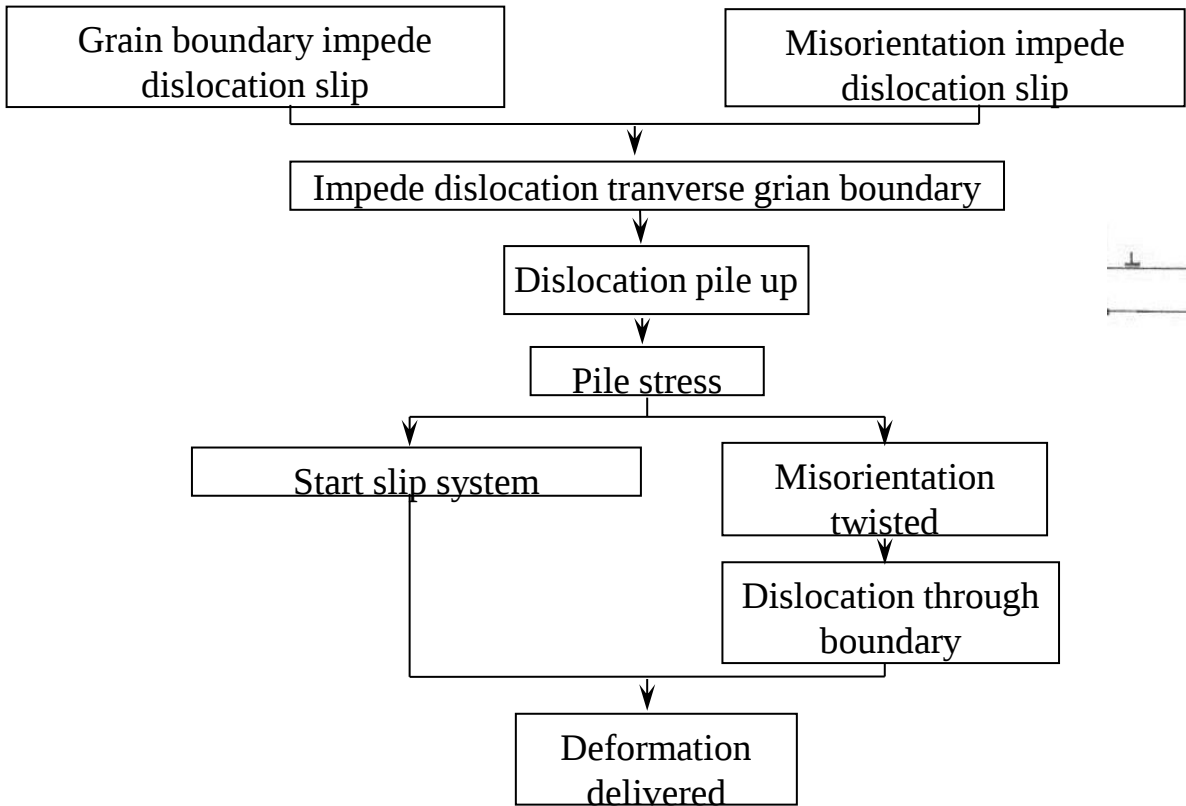
1.1 Single Crystal

- **Slip system:** A spatial orientation relationship consisting of a slip plane and slip direction.
- **Slip direction:** general happens at close stacking plane
- **Slip planes** are usually the most densely packed planes, and slip directions are usually the most densely packed directions.
- Under the same conditions, the more slip directions there are, the better the plasticity. And the more slip planes there are, the better the plasticity



	BCC	FCC	HCP
Slip Plane	{110}	{111}	{0001}
Slip Direction	<111>	<110>	< 11 $\bar{2}$ 0 >

1.2 Polycrystalline { misorientation
grain boundary

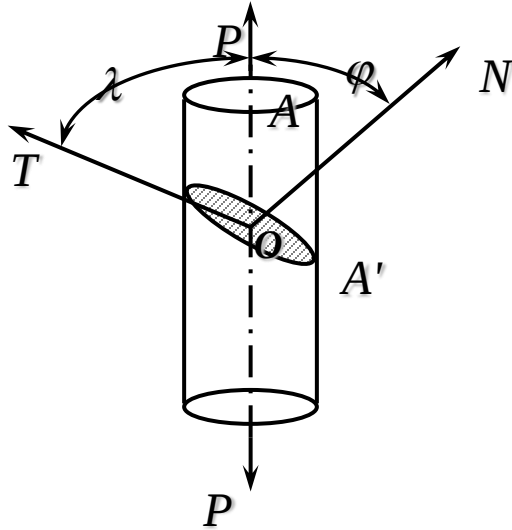


$$\tau_0 = n \tau$$

Dislocation Pile Up

1.3 Critical Shear Stress

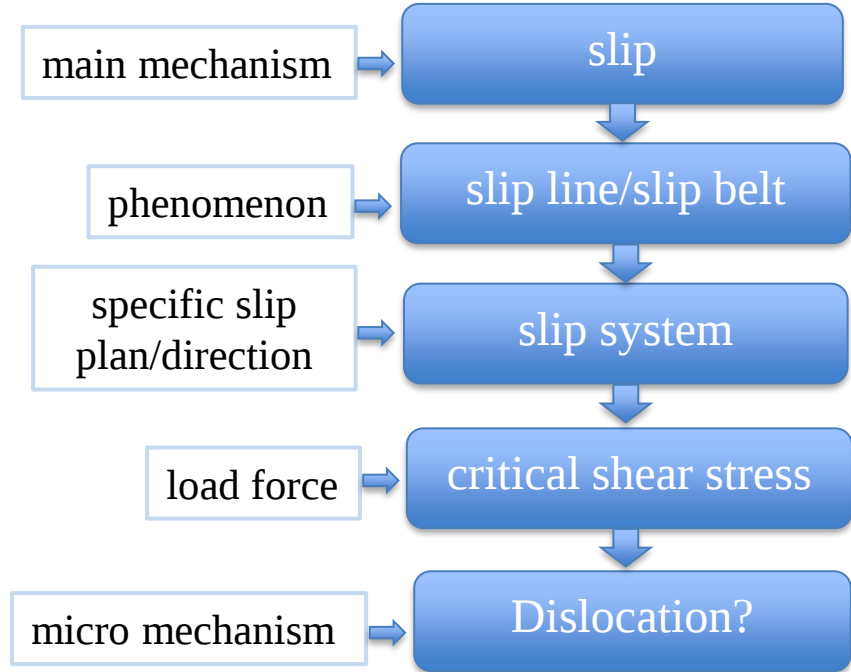
minimum shear stress to start slip



φ — load slip plane in normal direction

λ — load slip direction

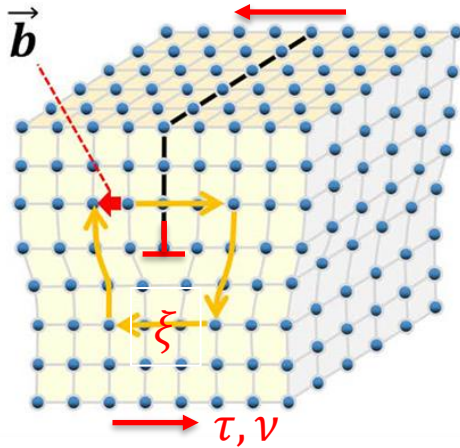
$$\tau = \sigma \cos \lambda \cos \varphi$$



2. Dislocation

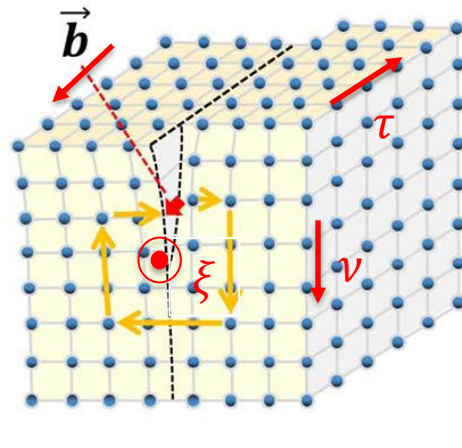
2.1 Definition: the boundary of slipped and un-slipped regions in the slip plane

Classification: edge, screw, mix



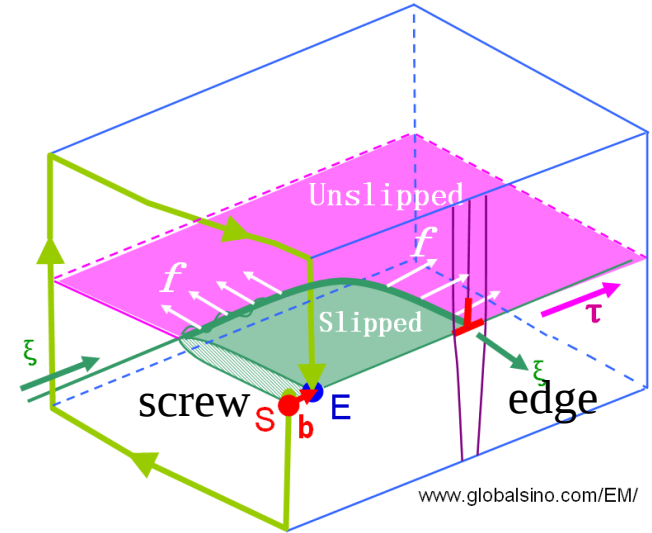
$$\tau \parallel \nu \parallel \bar{b}; \bar{b} \perp \xi$$

Edge $\bar{b} \perp \xi$



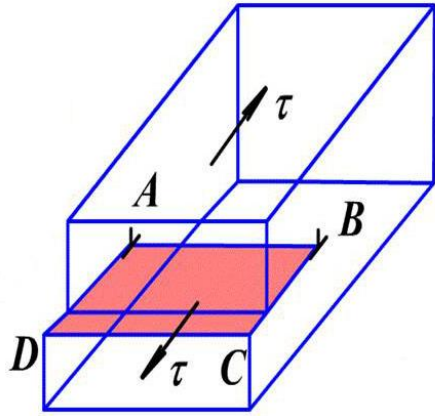
$$\xi \parallel \tau \parallel \bar{b}; \bar{b} \perp \nu$$

Screw $\bar{b} \parallel \xi$



Mix

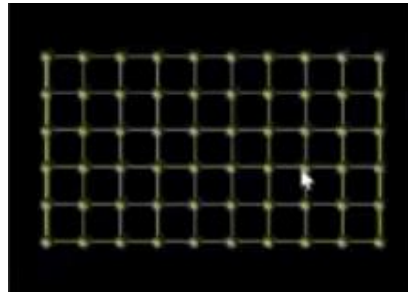
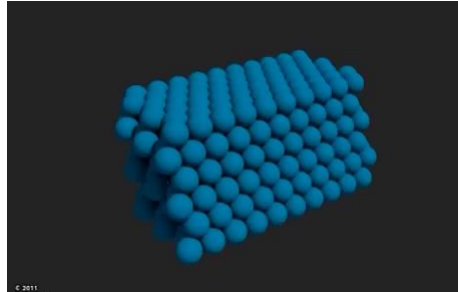
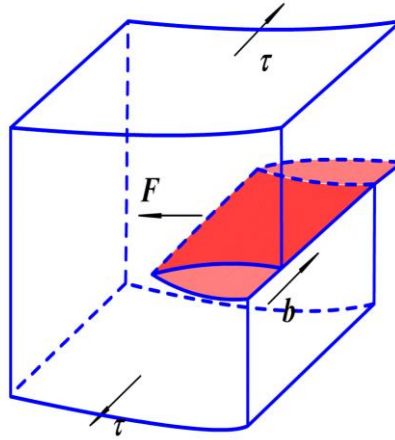
2.2 Force on



$$F = \tau * b$$

τ is the shear stress on the Burgers vector

b is the Burgers vector



Dislocation density

- Dislocation length in unit volume

$$\rho = \frac{S}{V} \quad \text{m/m}^3$$

- Dislocation length per cross section area

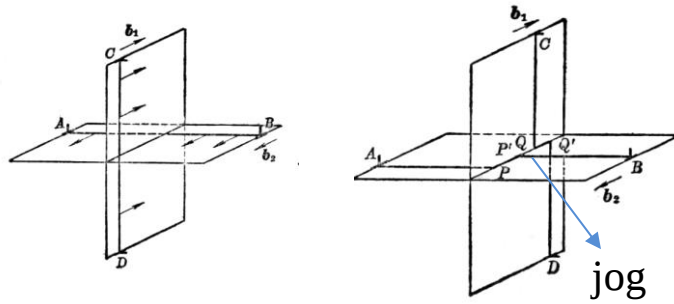
$$\rho = \frac{n}{A} \quad \text{1/m}^2$$



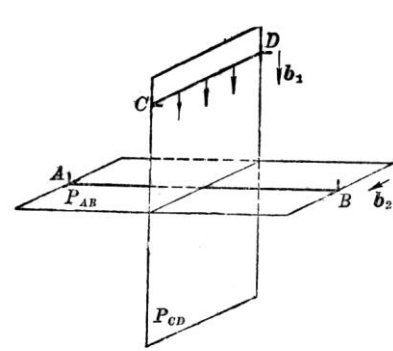
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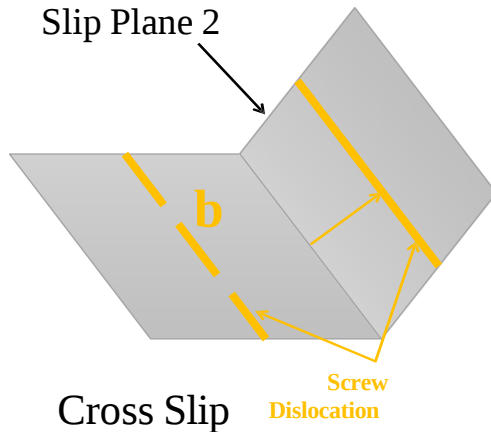
2.3 Dislocation Mobility and Interaction



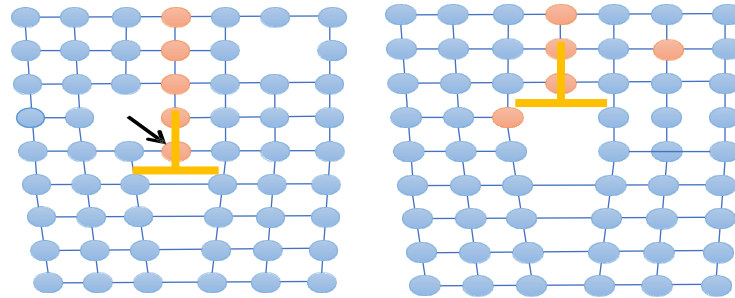
Parallel B interception of edge dislocation



Vertical B interception of edge dislocation



Cross Slip



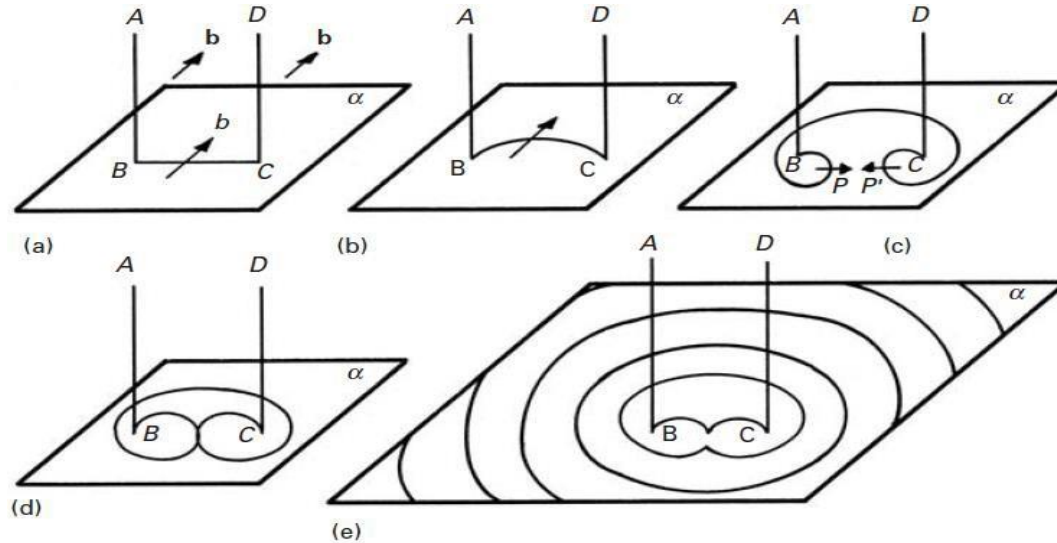
Dislocation Climb



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2.4 Dislocation Generation: Frank-Read



$$\tau = \frac{G * b}{l}$$

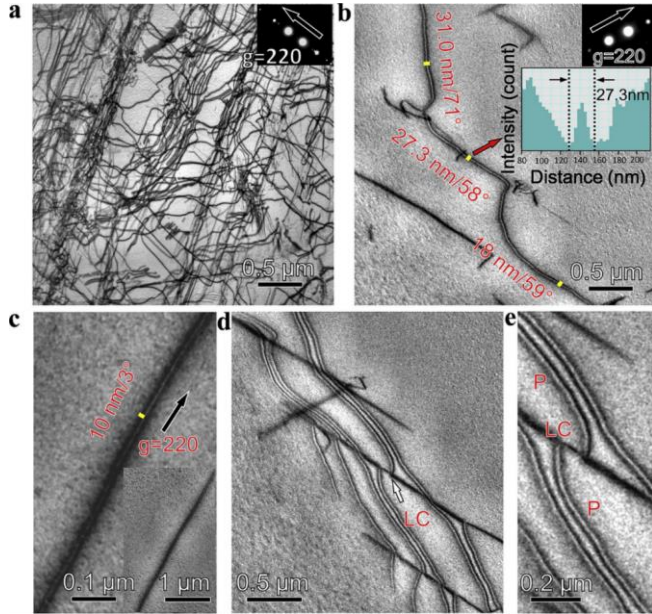
B:burgers vector

L: length of dislocation



Part 2 Dislocation Study Approaches

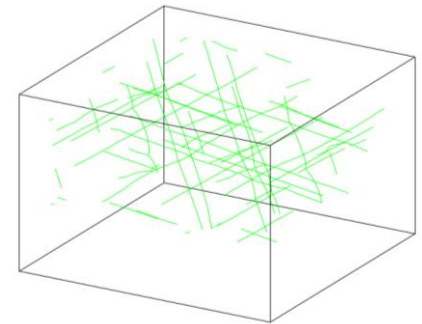
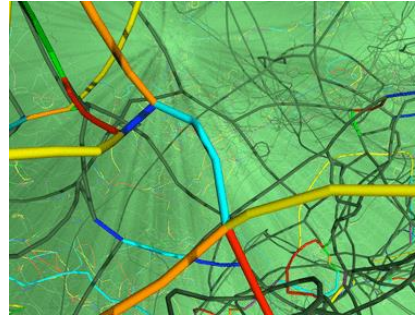
1. Experimental: TEM



2. Simulation

- **Discrete Dislocation Dynamics (DDD)**
- Phase Field Method
- Finite Element Method (FEM)
- Molecular Dynamics (MD)
- Continuum Dislocation Dynamics (CDD)
- Crystal Plasticity Finite Element Method (CPFEM)

Reason: closer to the real situation by space discrete and time step

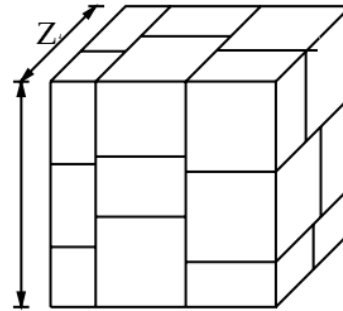
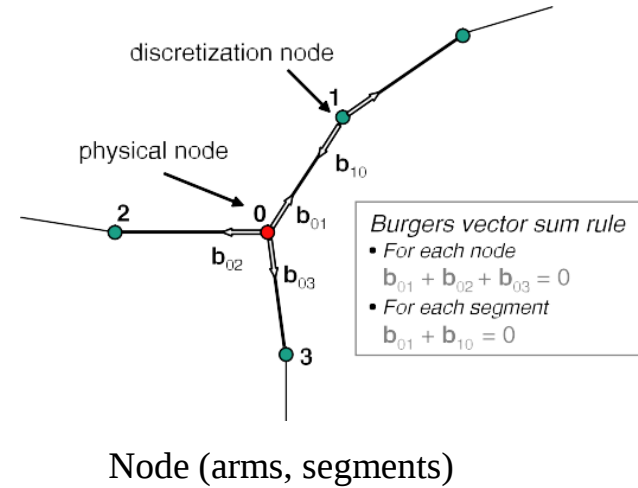


loop radius is $r_l = 5 \text{ nm}$

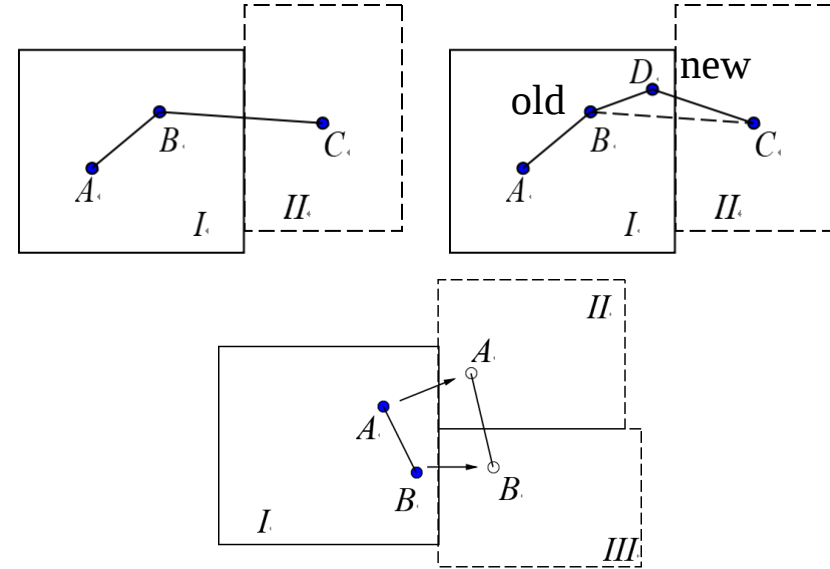
Precipitate size parameter is $R_p = 5 \text{ nm}$

Part 3 Discrete Dislocation Dynamics (Parallel Dislocation Simulator)

3.1 Discrete Dislocation Calculation Principle

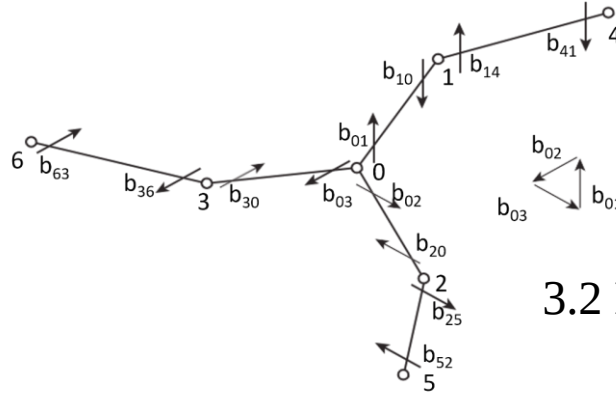


Domains
 $3 \times 3 \times 2$



MPI: Message Passing Interface(nodes)

3.2 Mobility



3.1 Force

$$\vec{f}_i = - \frac{\partial E(\{N_i\})}{\partial \vec{r}_i}$$

$N_i = [\vec{r}_i; \vec{b}_{ij}, j = 1, 2, \dots, n_i]$, where n_i is the connectivity of node i ;

$E(\{N_i\})$, is the total elastic energy of dislocation network

$$\partial E(\{N_i\}) \sum_{\langle i, j \rangle} W_s(ij) + \frac{1}{2} \sum_{\langle i, j \rangle; \langle k, l \rangle} W_l(ij, kl)$$

Where $W_s(ij)$ is the self energy of segments $\langle i, j \rangle$

$W_l(ij, kl)$ is the interaction energy between segments $\langle i, j \rangle$ and $\langle k, l \rangle$

3.2 Mobility Laws

$$F = \tau * b \quad M = \frac{v}{F} \quad M = \frac{v}{\tau * b}$$

M : the mobility function of velocity v of dislocation in response to the driving force f , $1/(\text{Pa} \cdot \text{s})$

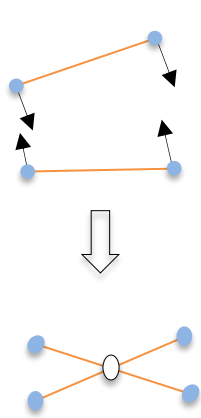
v : dislocation velocity m/s ;

b : Burgers length, $2.75 \times 10^{-10} \text{ m}$; (BCC)4

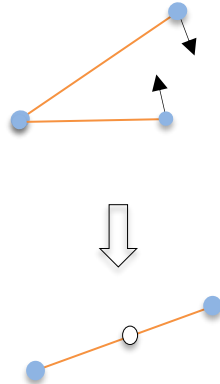
τ : shear stress on the Burgers vector, Pa

F : force on the dislocation, $\text{Pa} \cdot b$

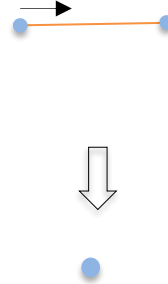
3.3 4 types dislocation event detection



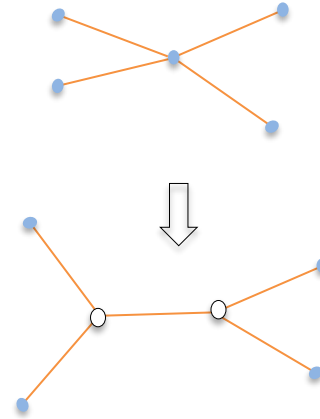
collision



zipping



shrinking



dissociation

Part 4 Preliminary Results

Initial dislocation cube and running parameters of mobility and stress set

Initial parameters set up	
Dislocation type	Screw
Cube length	3500 (b)
Maximum length	500 (b)
No. chains	100
Node count	1400
Dis density	1400 (mm ⁻²)

numXdoms	1	mobilityLaw	FCC_linear	Unit
numYdoms	1	shearModulus	2.70E+10	Pa
numZdoms	1	pois	0.347	
numXcells	4	YoungModulus	7.27E+10	Pa
numYcells	4	burgMag	2.86E-10	b
numZcells	4	MobEdge	-	pa ⁻¹ *s ⁻¹
maxSeg	500 (b)	MobScrew	-	pa ⁻¹ *s ⁻¹
minSeg	100 (b)	MobClimb	-	pa ⁻¹ *s ⁻¹
BoundType	Periodic/free	appliedStress	-	Pa
enableCrossSlip	Enabled	loadType	constant strain rate/stress	
maxstep	5000	edotdir	[1,0,0]	



Part 4 Preliminary Results

4.1 Frank Reed Dislocation Resource

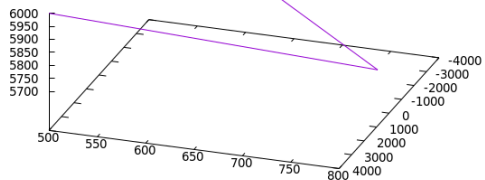
Initial dislocation condition set	
Dislocation type	Screw
Cube length	3500 (b)
Maximum length	500 (b)
No. chains	2
Node count	22
Dis density	3.1E12 (mm ⁻²)

Initial running parameters set				
numXdoms	1	mobilityLaw	FCC_linear	Unit
numYdoms	1	shearModulus	2.70E+10	Pa
numZdoms	1	pois	0.347	
numXcells	4	YoungModulus	7.27E+10	Pa
numYcells	4	burgMag	2.86E-10	b
numZcells	4	MobEdge	1.0E4	pa ⁻¹ *s ⁻¹
maxSeg	500 (b)	MobScrew	1.0E4	pa ⁻¹ *s ⁻¹
minSeg	100 (b)	MobClimb	-	pa ⁻¹ *s ⁻¹
BoundType	Periodic/free	appliedStress	1.0E+08	Pa
enableCrossSlip	Enabled	loadType	constant strain rate/stress	
maxstep	5000	edotdir	[1,0,0]	

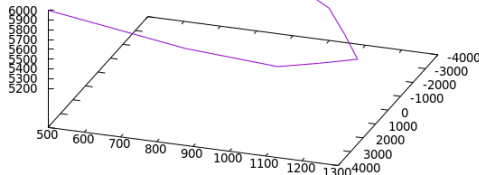


Frank-Reed dislocation case

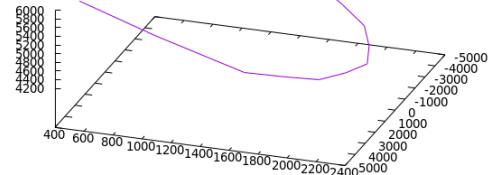
"/opt/data/paradis/ParaDis/tests/frank_read_src_results/gnuplot/0t0001"



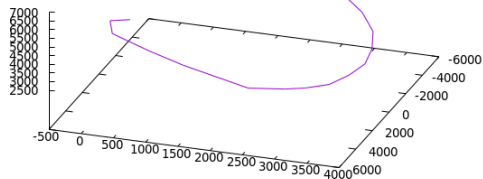
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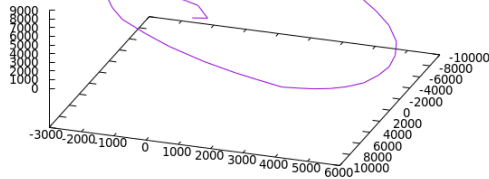
"/opt/data/paradis/ParaDis/tests/frank_read_src_results/gnuplot/0t0010"



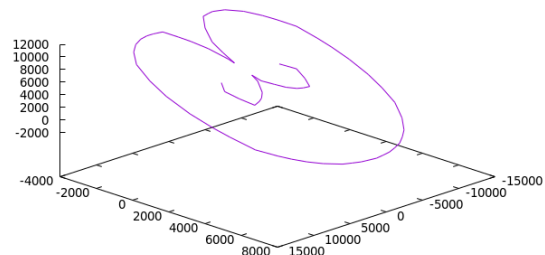
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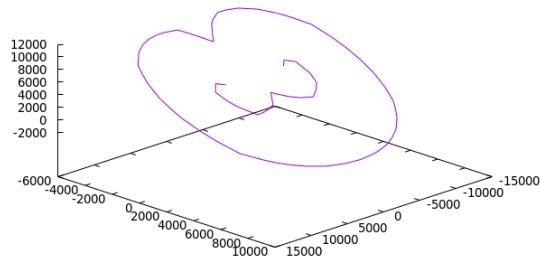
"/opt/data/paradis/ParaDis/tests/frank_read_src_results/gnuplot/0t0050"



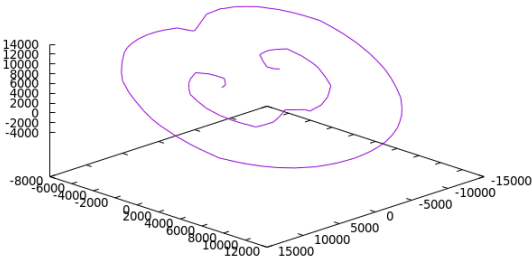
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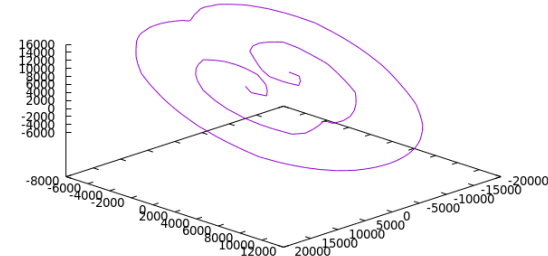
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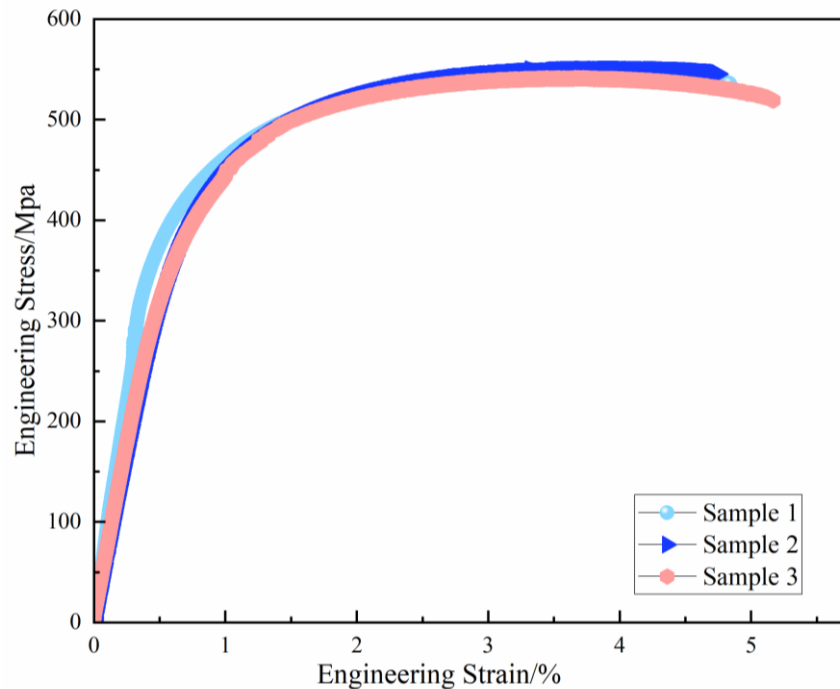


4.2 Aluminum uniaxial & creep simulation case

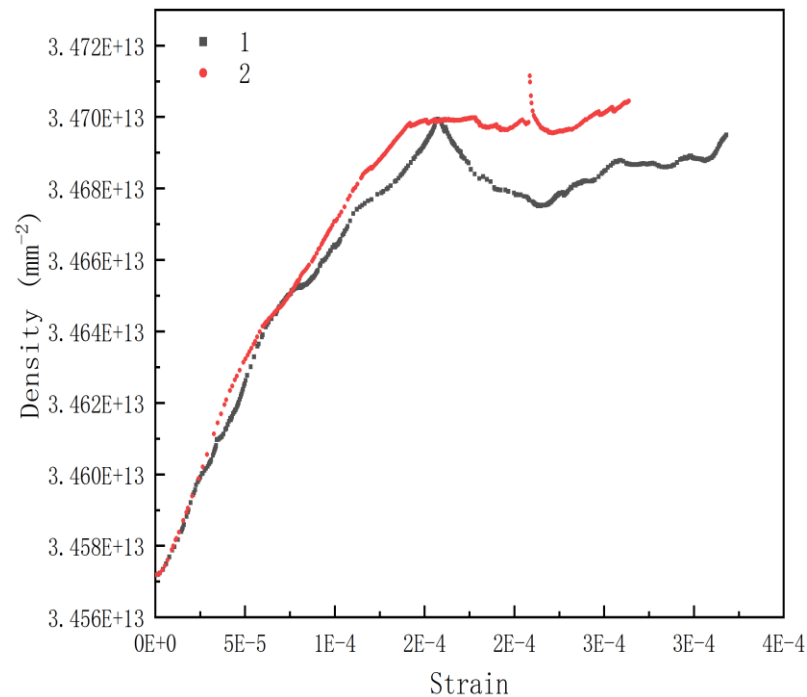
No.	Load type	Erate	Applied Stress	MobEdge	MobScrew	MobClimb	Steps set	Step stop by
Tensile 1	Uniaxial (constant strain rate)	1.0E+03	1.0E+08	1.0E+04	1.0E+04	100	50000	50000
Tensile 2	Uniaxial (constant strain rate)	1.0E+03	1.0E+07	1.0E+04	1.0E+04	100	50000	6276
Creep 1	Creep (constant stress)	1.0	1.0E+08	1.0E+04	1.0E+04	100	50000	3680
Creep 2	Creep (constant stress)	1.0	5.0E+07	1.0E+04	1.0E+04	100	50000	3996



Uniaxial (tensile)



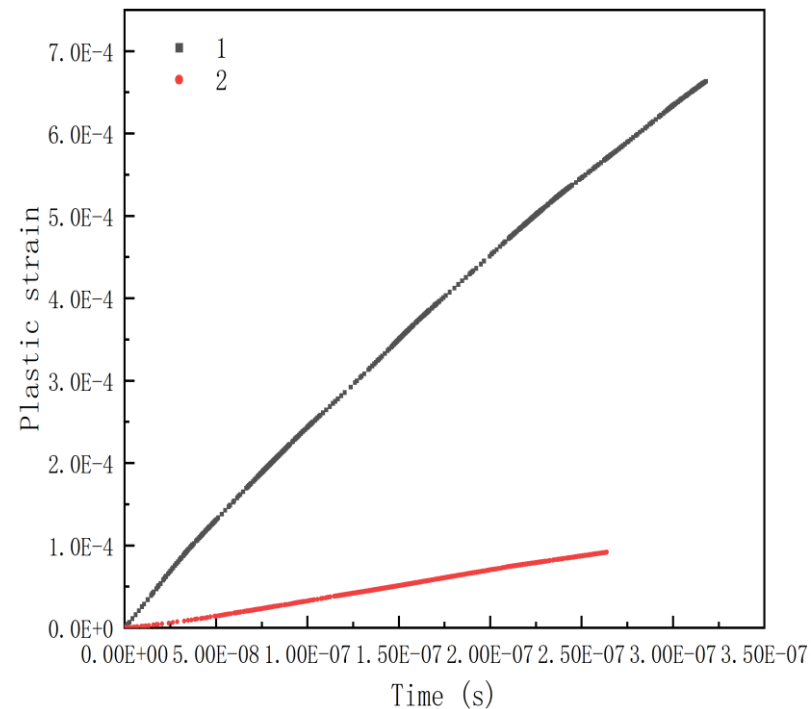
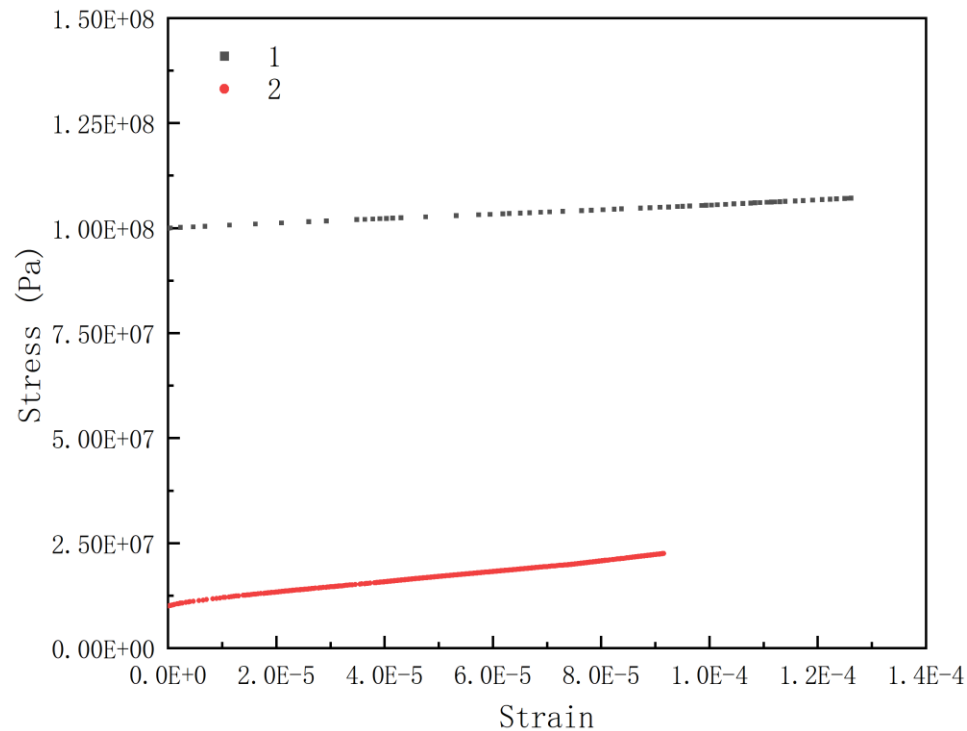
Al-Ce-Zr tensile test at room temperature



AppliedStress: 1) $1.0\text{E}+08$; 2) $1.0\text{E}+07$

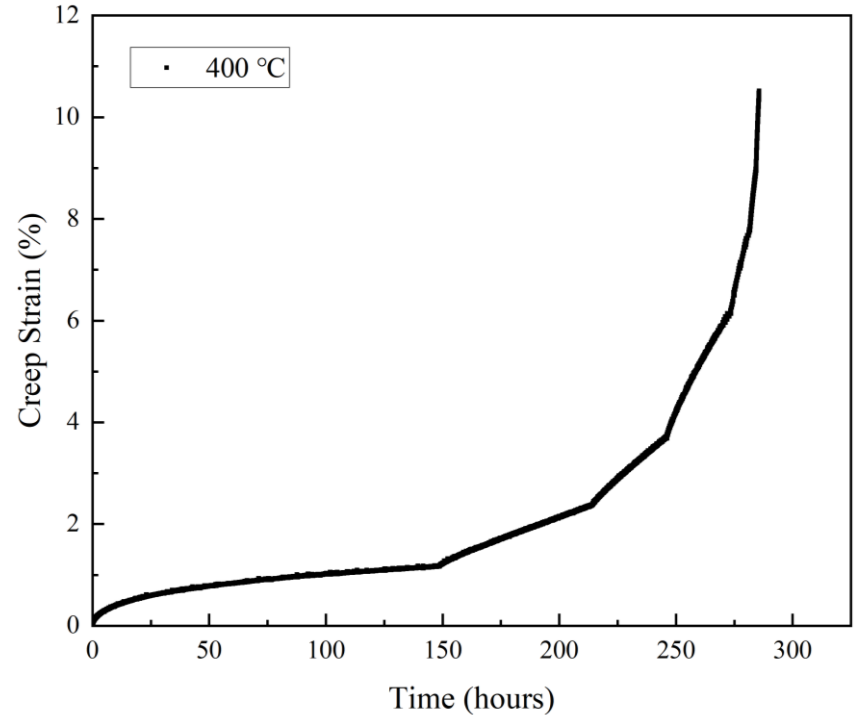
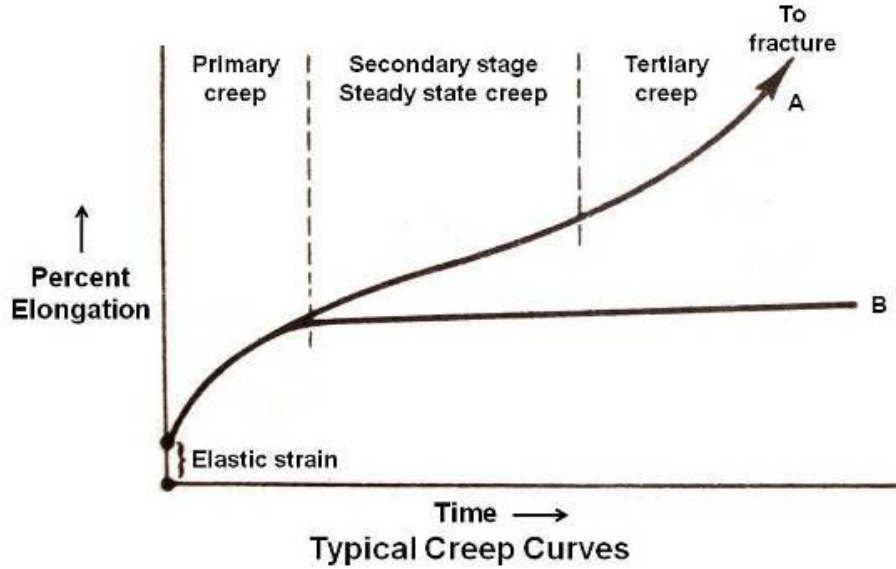


Uniaxial (tensile)

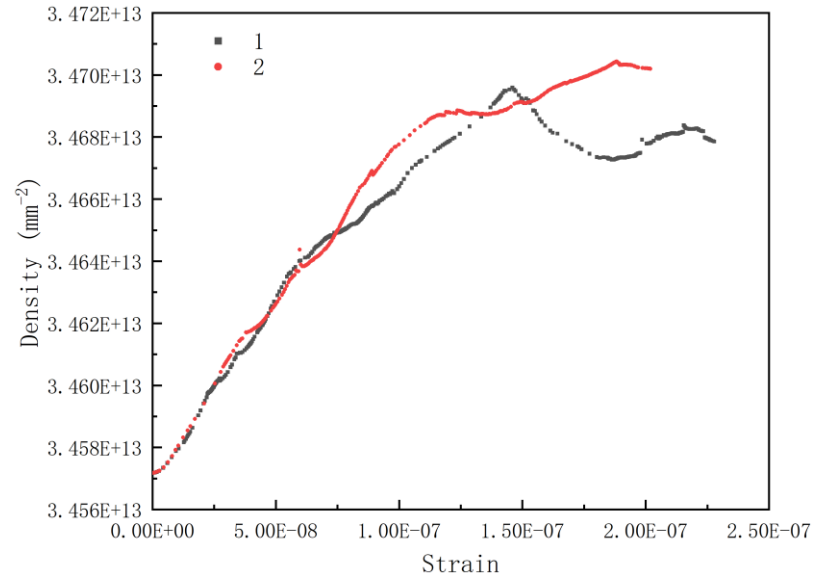
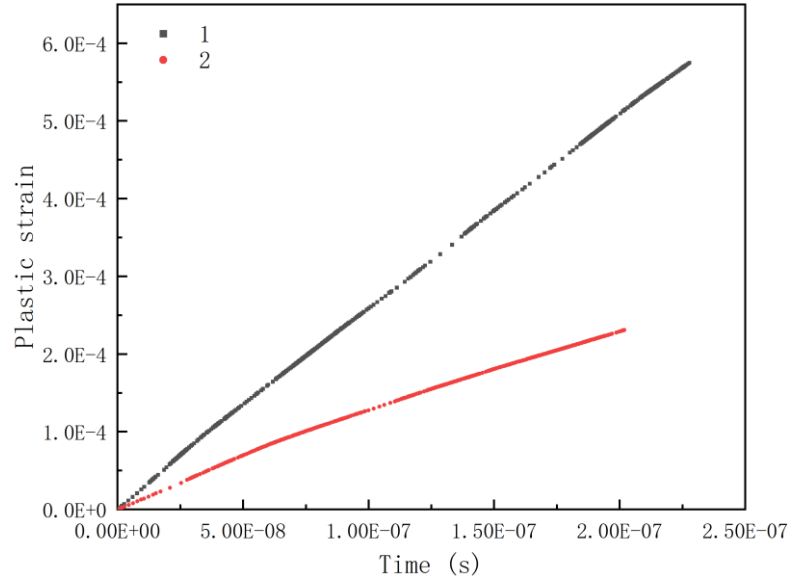


AppliedStress: (1) 1.0E+08; (2) 1.0E+07

Creep



Al-Ce-Mg Creep test at 400 C



AppliedStress: (1) 1.0E+08; (2) 5.0E+07



Thank you



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